

**Technical proposal for Boiling house**  
**Equipment for expansion of Sugar plant 2500**  
**TCD to 5500 TCD**

# **I N D E X**

<b>Sr. No.</b>	<b>PARTICULAR</b>
<b>1</b>	<b>PRAPOSED STEAM AND MASS BALANCE FOR 5500 TCD</b>
<b>2</b>	<b>EXISTING &amp; PRAPOSED EVAPORATOR BODIES + JUICE HEATER ARRANGEMENT</b>
<b>3</b>	<b>MATERIAL BALANCE SHEET</b>
<b>4</b>	<b>EXISTING &amp; PROPOSED EQUIPMENT LIST</b>
<b>5</b>	<b>EXISTING AND PRAPOSED BOILING HOUSE PUMP LIST</b>

## 01) HEAT MASS BALANCE OF 5500 TCD (240TCH) SUGAR PLANT

Absolute pressure and pressure drop

Exhaust condition: - 2.033 kg/cm<sup>2</sup> (120 Deg C)

Last body vacuum: - 0.204 (24'' vacuum) kg/cm<sup>2</sup>

Corresponding pressure/temp. Distribution of quintuple. Total pressure drop = 2.033 - 0.204 = 1.828 kg/cm<sup>2</sup>

- 1) Pressure drop in 1<sup>st</sup> body =  $11/50 \times 1.828 = 0.402$  kg/cm<sup>2</sup>
- 2) Pressure drop in 2<sup>nd</sup> body =  $10.5/50 \times 1.828 = 0.384$  kg/cm<sup>2</sup>
- 3) Pressure drop in 3<sup>rd</sup> body =  $10/50 \times 1.828 = 0.366$  kg/cm<sup>2</sup>
- 4) Pressure drop in 4<sup>th</sup> body =  $9.5/50 \times 1.828 = 0.347$  kg/cm<sup>2</sup>
- 5) Pressure drop in 5<sup>th</sup> body =  $9/50 \times 1.828 = 0.329$  kg/cm<sup>2</sup>

Then,

- 1) Absolute pressure in 1<sup>st</sup> body =  $2.033 - 0.402 = 1.631$  kg/cm<sup>2</sup>
- 2) Absolute pressure in 2<sup>nd</sup> body =  $1.631 - 0.384 = 1.246$  kg/cm<sup>2</sup>
- 3) Absolute pressure in 3<sup>rd</sup> body =  $1.246 - 0.366 = 0.881$  kg/cm<sup>2</sup>
- 4) Absolute pressure in 4<sup>th</sup> body =  $0.881 - 0.347 = 0.533$  kg/cm<sup>2</sup>
- 5) Absolute pressure in 5<sup>th</sup> body =  $0.533 - 0.329 = 0.204$  kg/cm<sup>2</sup>

Corresponding pressure/temp. of quintuple are

I - 1.631 / 113.24°C, II - 1.246 / 105.308°C, III - 0.881 / 95.6°C, IV - 0.533 / 82.548°C, V - 0.204 / 60.371°C,

Corresponding latent heat are

Exhaust : 538.725 I - 541.117 II - 544.128 III - 548.109 IV - 553.89 V - 564.634

A Masecuite produced =  $250 \times 28.362/100 = 70.904$  T/ Hr = 70904 Kg/ Hr.

Vapour required For A Masecuite =  $0.45 \times 70904 = 31907$  Kg/Hr.

B Masecuite produced =  $250 \times 12.019 / 100 = 30.047$  Ton/ Hr = 30047 Kg/ Hr.

Vapour required For B Masecuite =  $0.4875 \times 30047 = 11718$  kg/Hr

C Massecuite produced =  $250 \times 6.331/100 = 15.827 \text{ Ton/ Hr} = 15827 \text{ Kg/ Hr}$ .

Vapour required For C Massecuite =  $0.48 \times 15827 = 6647 \text{ kg/Hr}$

Mix juice % cane = 100.079 %

Mix juice produced per hour =  $5500/22 = 250 \text{ Ton / hr} = 250000 \text{ kg/hr}$ .

Filtrate % cane = 14.2%

Sulphured juice % cane = 115.929%

Sulphured juice produced =  $250 \times 1.15929 = 289.824 \text{ ton /hr} = 289824 \text{ kg/hr}$

- A) Vapour required for 1<sup>st</sup> raw juice heating from 32 deg. to 42deg.  
in vapour line juice heater by last body vapour  
=  $250000 \times 0.9 \times (42-32) / 564.634$   
= 4041 Kg/Hr

- B) Water required for 2<sup>nd</sup> raw juice heating from 42°C to 55°C by Hot condensate in

Condensate juice heater

=  $250000 \times 0.9 \times (55-42) / (101-60) = 71341 \text{ kg/hr} = 71.34 \text{ T/hr}$

- C) Vapour required for 3<sup>rd</sup> raw juice heating from 55 deg. to 72deg.  
in Tubular juice heater by 4th Body vapour  
=  $250000 \times 0.9 \times (72-55) / 548.109 = 7076.00 \text{ kg / hr}$

- D) Vapour required for 1<sup>st</sup> Sulphured juice heating from 70°C to 85°C  
by 2<sup>nd</sup> body vapour in Tubular juice heater  
=  $289824 \times 0.9 \times (85-70) / 544.128 = 7286 \text{ kg / hr}$

- E) Vapour required for 2<sup>nd</sup> Sulphured juice heating from 85°C to 102°C  
by 1<sup>st</sup> body vapour in Tubular juice heater  
=  $289824 \times 0.9 \times (102-85) / 541.117 = 8303 \text{ kg/hr}$

- F) Vapour required for Clear juice heating from 96°C to 103°C by  
1<sup>st</sup> body vapour

$$= 252324 \times 0.9 \times (110-96) / 541.117 = 2977 \text{ kg/hr}$$

G) Vapour required for Clear juice heating from 103°C to 110°C by Exhaust steam

$$= 252324 \times 0.9 \times (110-103) / 538.725 = 2990 \text{ kg/hr}$$

$$\text{Vapour produced by 5}^{\text{th}} \text{ body} = X + 4041$$

$$\text{Vapour produced by 4}^{\text{th}} \text{ body} = X + 4041$$

$$\text{Vapour produced by 3}^{\text{rd}} \text{ body} = X + 4041 + 7076$$

$$\text{Vapour produced by 2}^{\text{nd}} \text{ body} = X + 4041 + 7076 + 7286 + 31907 + 11718$$

$$\text{Vapour produced by 1}^{\text{st}} \text{ body} = X + 4041 + 7076 + 7286 + 31907 + 11718 + 8303 + 2977 + 6647$$

$$\text{Total vapour produced} = 5X + 161182$$

$$\text{Total evaporation} = 252324 (60 - 14.42 / 60) = 191673 \text{ kg/hr}$$

$$5X + 161182 = 191673 \quad X = 6098 \text{ kg/hr}$$

$$1) \text{ Vapour produced by 5}^{\text{th}} \text{ body} = 10139 \text{ Kg/Hr}$$

$$2) \text{ Vapour produced by 4}^{\text{th}} \text{ body} = 10139 \text{ Kg/Hr}$$

$$2) \text{ Vapour produced by 3}^{\text{rd}} \text{ body} = 17215 \text{ Kg/Hr}$$

$$3) \text{ Vapour produced by 2}^{\text{nd}} \text{ body} = 68127 \text{ Kg/Hr}$$

$$4) \text{ Vapour produced by 1}^{\text{st}} \text{ body} = 86053 \text{ Kg/Hr}$$

Then

$$A) \text{ Heating surface of 1}^{\text{st}} \text{ body} - 86053 / 27 = 3187 \approx 3200 \text{ m}^2 \text{ approximate}$$

$$B) \text{ Heating surface of 2}^{\text{nd}} \text{ body} - 68127 / 22 = 3097 \text{ m}^2 \approx 3100 \text{ m}^2 \text{ approximate}$$

$$C) \text{ Heating surface of 3}^{\text{rd}} \text{ body} - 17215 / 17 = 956 \approx 1000 \text{ m}^2 \text{ approximate}$$

$$D) \text{ Heating surface of 4}^{\text{th}} \text{ body} - 10139 / 15 = 676 \approx 700 \text{ m}^2 \text{ approximate}$$

E) Heating surface of 5<sup>th</sup> body –  $10139/15 = 676 \approx 650$  m<sup>2</sup> approximate

$$\begin{aligned}\text{Steam \% cane} &= (86053/250) \times 100 \\ &= 34.421\%\end{aligned}$$

Consider 2.0 % extra steam required for CJ2 Heating, Pan Body wash, Seed melting, Soda Boiling, Drain & Line Losses etc.

Steam % on Cane Will be = 36.421 %

Brixes in Quintuple bodies

1. 1<sup>st</sup> Effect Evaporator Body

$$\begin{aligned}B \times J &= B1 \times J1 \\ 14.422 \times 252.324 &= B1 \times (252.324 - 86.053)\end{aligned}$$

$$B1 = 21.886$$

2. 2<sup>nd</sup> effect Evaporator Body

$$\begin{aligned}B1 \times J1 &= B2 \times J1 \\ 21.886 \times 166.27 &= B2 \times (166.27 - 68.127)\end{aligned}$$

$$B2 = 37.079$$

3. 3<sup>rd</sup> Effect Evaporator Body

$$\begin{aligned}B2 \times J2 &= B3 \times J3 \\ 37.079 \times 98.144 &= B3 \times (98.144 - 17.215)\end{aligned}$$

$$B3 = 44.966$$

4. 4<sup>th</sup> Effect Evaporator Body

$$B3 \times J3 = B4 \times J4$$

$$44.966 \times 80.928 = B4 \times (80.928 - 10.139)$$

$$B4 = 51.406$$

5. 5<sup>th</sup> Effect Evaporator Body

$$B4 \times J4 = B5 \times J5$$

$$51.406 \times 70.790 = B5 \times (70.790 - 10.139)$$

$$B5 = 60.00$$

#### AVERAGE BRIXES IN QUINTUPLE EVAPORATOR BODIES

Raw Juice Brix = 14.422

1. 1<sup>st</sup> Effect Evaporator Body

$$= \frac{14.422 + 21.886}{2}$$

$$B1 = 18.154$$

2. 2<sup>nd</sup> effect Evaporator Body

$$= \frac{21.886 + 37.079}{2}$$

$$B2 = 29.482$$

$$\begin{aligned} & 3. \text{ 3}^{\text{rd}} \text{ Effect Evaporator Body} \\ & \quad 37.079 + 44.966 \\ = & \frac{\text{-----}}{2} \end{aligned}$$

$$B3 = 41.022$$

$$\begin{aligned} & 4. \text{ 4}^{\text{th}} \text{ Effect Evaporator Body} \\ & \quad 44.966 + 51.406 \\ = & \frac{\text{-----}}{2} \end{aligned}$$

$$B4 = 48.186$$

$$\begin{aligned} & 5. \text{ 5}^{\text{th}} \text{ Effect Evaporator Body} \\ & \quad 51.406 + 60 \\ = & \frac{\text{-----}}{2} \end{aligned}$$

$$B5 = 55.703$$

## 2)EXISTING AND PRAPOSED EVAPORATOR AND JUICE HEATER ARRANGEMENT

### Evaporators

EXISTING		PROPOSED		Remark
WORKING	STANDBY	WORKING	STANDBY	
2,800	NIL	2,800	3,800	2New FFE
2,500	NIL	2,500		
900	700	900	700+560	Nil
560	560	560	560	Nil
440	440.000	440	440	Nil

### JC Heaters

Heating	EXISTING		PROPOSED		New
	WORKING	STANDBY	WORKING	STANDBY	
RJ1	350 M2	350M2	350M2	350M2	Nil
RJ2	NIL	NIL	170M2	170M2	Re arrange
RJ3	170M2	170M2	170M2	350	3 x 350 M2 New heaters
SJ1	170M2		350		
SJ2	170M2		350		
CJ1	170M2	NIL	170M2	350	Re arrange & 1 new 350 M2 heater
CJ2	NIL	NIL	170M2		

### 3) Material balance sheet

CRUSHING CAPACITY	5,500.00	TCD	250.00	TCH	POL BALANCE		PARTICULARS	SOLIDS(MT)	% BRIX	% PURITY	SOLIDS T/HR	QUANT % CANE
			0.00	TPH	POL IN CANE	13.04	SYRUP	14.84	60.00	84.00	37.11	24.74
Recovery% Cane	10.90				POL IN MJ	12.34	A MASSECUITE	25.81	91.00	88.00	64.52	28.36
					POL IN BAGASSE	0.70	A HEAVY	11.58	80.00	74.00	28.96	14.48
Material	Purity	Material	Purity		POL IN FC	0.10	A LIGHT	0.60	75.00	88.00	1.49	0.80
Syrup	84.00	Raw Sugar			POL IN FM	1.26	A SUGAR	13.63	99.98	99.90	34.07	13.63
White Sugar	99.90				POL UNDETERR	0.10	AFW SUGAR	14.23	99.40	99.40	35.56	14.31
A Massecuite	88.00	A Heavy Molasses	74.00		TOTAL LOSS	2.16	B MASSECUITE	11.30	94.00	75.00	28.24	12.02
B Massecuite	75.00	A Light Molasses	88.00				B HEAVY	5.09	80.00	53.00	12.73	6.37
C Massecuite	55.00	B Heavy Molasses	53.00		RECOVERY	10.90	B SUGAR	5.92	90.00	95.00	14.79	6.58
AFW	99.40	C light	60.00				C MASSECUITE	6.33	100.00	55.00	15.83	6.33
B Sugar	95.00	Final Molasses	35.00				C LIGHT	0.95	78.00	60.00	2.38	1.22
CFW	82.00						FINAL MOLASSES	3.64	88.00	35.00	9.09	4.13
CAW	94.00						CFW SUGAR	2.69	96.00	82.00	6.73	2.81
							CAW SUGAR	1.74	95.00	94.00	4.36	1.83
							DRY SEED	2.42	90.00	-	6.05	2.69
Solid in Syrup		14.84					MELT	13.04	65.00	95.00	32.60	20.06
Total Solids in Syrup		37.11					Total Massecuite% Cane					46.71

### 4)EXISTING & PROPOSED EQUIPMENT LIST

Sr. No	Equipment particulars	Existing		Required as per 5500 TCD		REMARK
		Working	Spare	Working	Spare	
1	Juice Flow Stabilization	Not Mentioned		one Set		
2	Raw Juice receiving tank	Not Mentioned				
3	Mass Flow meter	350T/HR	Nil	350T/HR	No Need	
4	Imbibition water tank	Not Mentioned		17M3 Tank		
5	Juice heaters					
	1) VLJH ( Tubular)	350 M2 x1No's	350 M2 x1No's	350 M2 x1No's	350 M2 x1No's	
	2) Condensate R.JC heater ( Duplex heater)	Nil	Nil	170M2 x1 No's	170M2 x 1 No's	Existing JH re arranged
	3) R.JC 3rd heating ( Tubular)	170M2 x1 No's	170M2 x1 No's	170M2 x1 No's	350M2	350M2 x 3 No's New Heaters used for a RJ3/SJ1/SJ2 heating
	S.JC 1st heating ( Tubular)	170M2 x1 No's		350M2		
	S.JC 2nd heating ( Tubular)	170M2 x1 No's		350M2		
	Cl.Juice heater ( Tubular)	170M2 x1 No's	Nil	170M2 x1 No's	350M2 x1 No's	Spare 350M2 heater used for CJ1/CJ2 heating
	Cl Jc 2nd Heating	Not Mentioned	Not available	170M2 x1 No's		
6	Juice sulphitor	300 HL		300HL		Existing is Suitable
7	Juice sulphitor Auto pH control system	Not Mentioned		Single loop Auotamtion with Suitable capacity required		
8	Sulphured Juice Receiving Tank	Not Mentioned		45 M3 Capacity tank required		
9	Sulphur Burners					
	Juice side	140Kg/Hr	140Kg/Hr	200	140 Kg/Hr	New 200 kg/hr FTSB required

	<b>Syrup side</b>	70 Kg/Hr	70 Kg/Hr	70 Kg/Hr	70 Kg/Hr	
10	<b>Air Blowers</b>					
	<b>Juice side</b>	846 M3/Hr		<b>924 M3/Hr</b>		New 1200M3/Hr Blower required
	<b>Syrup side</b>	600 M3/Hr x 2		<b>630 M3/Hr</b>	<b>630 M3/Hr</b>	Existing is Suitable
11	<b>Lime Slacker Unit</b>	1200 Kg/Hr		<b>1200 Kg/Hr</b>		Existing is Suitable
	<b>Lime cyclone</b>	Not Mentioned				SUITABLE FOR SLAKER CAPACITY required
	<b>Lime classifier</b>	Not Mentioned				
	<b>MOL Screening</b>	Not Mentioned		Suitable to screen 26M3/Hr MOL vibro x 2 No's needed		
	<b>MOL receiving tanks</b>	15 M3 x 2 no's				Existing is Suitable
	<b>Screened MOL Receiving tank</b>	Not Mentioned		<b>15 M2 x 1 No's tank required</b>		
12	<b>Juice clarifier</b>	410 M3	250M3			Existing is Suitable
		444 Type	444 Type			
13	<b>Clear Juice Receiving tank</b>	Not Mentioned		<b>32M3 X 1 No's Tank required</b>		
14	<b>Vacuum filter Filtering area</b>	236				
	<b>Vacuum filter</b>	8' X 16' = 36				Existing is Suitable
		10' x 20' = 56				
		16' x 32' = 144				
	<b>Mud tank</b>	Not Mentioned				
	<b>Filtrate tank</b>	Not Mentioned				
	<b>Filtrate pump</b>	Not Mentioned				

	<b>Cake wash tank</b>	Not Mentioned				
	<b>Cake wash pump</b>	Not Mentioned				
	<b>Mud Mixer</b>	Not Mentioned				
	<b>Bagacillo blower</b>	Not Mentioned				
	<b>Bagacillo cyclone</b>	Not Mentioned				
	<b>Inter connecting pipeline</b>	Not Mentioned				
	<b>Mud Pump</b>	Not Mentioned				
	<b>Barometric condenser</b>	Not Mentioned				
	<b>Vacuum pump</b>	Not Mentioned				
15	<b>Evaporator bodies</b>					
	<b>SK vessel</b>	2800 M2		3600		New 2No's x 3600M2 FFE Body as a 1st /2nd Effect required
	<b>1st/ 2nd Vessel</b>	2500 M2		3600/2800		
	<b>2nd vessel</b>			3600/2500		
	<b>3rd A vessel</b>	950		950		
	<b>3rd B vessel</b>	700		700+560		
	<b>4th A vessel</b>	560		560		
	<b>4th B vessel</b>	560		560		
	<b>Vth A Vessel</b>	440		440		
	<b>Vth B Vessel</b>	440		440		
16	<b>Un Sulphured syrup Receiving tank</b>			<b>3.14 M3 Reciever required</b>		
17	<b>Ev.set Multijet condenser</b>	Single entry x 2 No;s				Existing is Suitable
18	<b>Syrup Sulphitor</b>	120HL				Existing is Suitable
19	<b>Sulphured Syrup receiving tank</b>	Not Mentioned		<b>3.14 M3 Reciever required</b>		
20	<b>Syrup + molasses supply tanks</b>					

	<b>For Syrup</b>	18.75 M3 x 6 No's		<b>Additional 40 M3 x 2 Nos required</b>		
	<b>For A-Heavy Molasses</b>	8.24 M3 x 15 No's				
	<b>For B-Heavy Molasses</b>					
	<b>For C-Light Molasses</b>					
21	<b>Molasses conditioners</b>					
22	<b>Vacuum pans</b>					
	<b>A Pan</b>	40 T x 1 No's		<b>50T x 3 No's + 80 T x 2 Nos</b>		Existing pan rearranged
		50 T x 3 No's				
	<b>B Grain Pan</b>	40 T x 1 No's				Existing is Suitable
	<b>B Pan</b>	15 Mt/Hr		<b>15Mt/Hr x 1 nos + 40Mt x 1 no's</b>		
	<b>C Grain Pan</b>	80 T x 1 No's				Existing is Suitable
	<b>C Pan</b>	80 T x 1 No's		<b>New 15Mt/Hr Continuous Pan required</b>		
23	<b>Pan Condensate tank</b>	Not Mentioned		<b>6.0 M MS Tank required</b>		
24	<b>Pan Condensate pump</b>	Not Mentioned		<b>72T/Hr Pump x 2 No's Required</b>		
25	<b>Dry seed Crystallizer</b>	22M3		<b>One new 40 MT D.Cry required</b>		
26	<b>B seed Crystallizer</b>	18M3				<b>Both Existing D &amp; B Cry used</b>
27	<b>A VC</b>	54.44 MT				Existing is Suitable
28	<b>B VC</b>	25.87 T + 22.68 T				Existing is Suitable
29	<b>C VC</b>	33 MT				Existing is Suitable

30	<b>Molasses Conditioner</b>					
	<b>A Heavy</b>	4.62 Mt capacity		<b>Suitable capacity DCH Heater</b>		
	<b>B Heavy</b>	9.4 Mt Capacity		<b>Suitable capacity DCH Heater</b>		
	<b>C Light</b>	9.4 Mt Capacity		<b>Suitable capacity DCH Heater</b>		
31	<b>Condenser</b>			<b>Suitable for Exisitng Pans</b>		New Single entry condenser for new 15Mt/Her Conti pan
32	<b>Air cooled receiving crystallizers</b>					
	<b>For A-Masscuite receiving</b>	90 x 1 No's +55 x 2 No's		<b>80 x 2no's New crystalizers required</b>		
	<b>For B-Massecuite receiving</b>	30 x 4 No's + 150Mt MVC		30 x 4 No's + 150Mt MVC		
	<b>For C-Massecuite receiving</b>	30 x 2 No's + 200Mt MVC +120MVC		<b>Existing 150Mt C VC to be used for B M/C &amp; 120Mt VC use for C M/C</b>		
33	<b>Centrifugal machines</b>					
	<b>A Pugmill</b>	Not Mentioned				
	<b>Batch Machines For A M/C</b>	750kg/Cycle x 5 No's + 1750Kg/Cysl x 1 No's		<b>Machine capacity not mentioned properly</b>		
	<b>A Heavy Run off Tank</b>	Not Mentioned				
	<b>A Light Run off tank</b>	Not Mentioned				
	<b>A Heavy Run off Pump</b>	Not Mentioned				
	<b>A Light Run off pump</b>	Not Mentioned				
	<b>Continuous C/F</b>	Not Mentioned				

	<b>Machines</b>				
	<b>B Pugmill</b>	Dimension need			
	<b>For B Masseците</b>	8 Mt x 2 No's		<b>One new 15Mt capacity machine to be install</b>	
	<b>Bh Run off Tank</b>	Not Mentioned			
	<b>BH Pump</b>	Not Mentioned			
	<b>B Seed pump</b>	Not Mentioned			
	<b>For CFW</b>	6Mt x 3 No's			
	<b>For CAW / B Masseците</b>			<b>One new 15Mt capacity machine to be install</b>	
	<b>CFW Seed Pump</b>	Not Mentioned			
	<b>Magma mixer</b>	Dimension need			
	<b>For CFW magma</b>	6Mt x 2 No's		<b>One new 15Mt capacity machine to be install</b>	
	<b>CAW Pump</b>	Not Mentioned			
	<b>For CAW + B-Magma with partion plate</b>	Dimension need			
34	<b>Melter capcity</b>	15Mt		<b>To be modify to handle 40 Mt/Hr melt load</b>	
35	<b>Rori melter</b>	15 MT			<b>Existing is Suitable</b>
36	<b>Air Compressor</b>	2Nos x 1.43M3/Min capacity			
37	<b>Final Molasses Transfer Pump</b>	Not Mentioned			
38	<b>Sugar Hopper A</b>	4 No's x 1.5 mtr width			Existing is Suitable
39	<b>Hot Blower for A set</b>	5550 CFM			
40	<b>Cold Blower for A set</b>	5550 CFM			

41	<b>Sugar Hopper B</b>	3 No's x 2.0 mtr width				
42	<b>Hot Blower for A set</b>	6550 CFM				
43	<b>Cold Blower for A set</b>	6550 CFM				
44	<b>Sugar Elevator A</b>	30Mt/Hr				Existing is Suitable
45	<b>Sugar Elevator B</b>	40Mt/Hr				Existing is Suitable
46	<b>Sugar Grader A</b>	40Mt/Hr				
47	<b>Sugar Grader B</b>	10Mt/Hr		<b>1 No's 6 Dec 35 MT Grader is required</b>		
48	<b>Sugar Silo capacity</b>	Not Mentioned				
49	<b>Sugar Weighing Machine</b>	2 No's				Capacity not mentioned
50	<b>Sugar Bag Sticking machine</b>	2 No's of capacity 100 bag/Min				Speed to be rectify
51	<b>Cold Water Overhead tank capacity</b>	8.49	M3			
52	<b>Service water pump capacity</b>	Not Mentioned				
53	<b>Hot Water Overhead tank capacity</b>	11.64	M3			Existing is Suitable
54	<b>Hot Water Overhead tank capacity</b>	11.68	M3			Existing is Suitable

**5) EXISTING AND PRAPOSED BOILING HOUSE PUMP LIST**

**Expansion from 2500 TCD to 5500TCD**

	CANE – Tons	5500/ 250		Colour codes : Yellow - New Pumps to be procured									
				Green - Existing pumps used									
				Red - Points to be discussed									
			<b>EXISTING PUMPS</b>					<b>RE ARRANGEMENT FOR 200 TCH</b>					
Sl.No	DESCRIPTION OF THE PUMP	Make	NO. OF PUMPS	CAPACITY IN M <sup>3</sup> / Hr	HEAD	HP	RPM	NO. OF PUMPS	CAPACITY IN M3/Hr	HEAD	HP	RPM	REMARKS
1	Screened RJuice Pumps	PSP	2	250	45	100	1485	2	280	70	Suitable to pump capacity		New Pumps required
2	Exhaust Condensate Pumps For ( 2800 M2)	Sintech	2	80	40	30	1460	2	80	40	30	1460	New FFE 3600M2 Condensate conection to both 1&2 body condensate
3	2500 M2 body	Wilo	2	100	30	20	1460	2	100	30	20	1460	
4	3600M2 FFE Circulation pump							4	750	30			4 No's new pump required
5	900 M2 body	KPD	1	80	30	10	1455	1	80	30	10	1455	

6	700 M2 body	Wilo	1	10	25	3	1450	1	10	25	3	1450	560M2 body condensate connection to be given to 700M2 body condensate mond
7	4A Body	KPD	1	55	25	20	1450	1	55	25	20	1450	
8	4B Body	KPD	1	55	25	15	1450	1	55	25	15	1450	
9	5A Body	KPD	1	55	25	15	1450	1	55	25	15	1450	
10	5B Body	KPD	1	55	25	10	1450	1	55	25	10	1450	
11	VLJH Condensate pump			Not Given									If avaiable existng used
12	JH No 01 Condensate	Wilo	1	10	25	3	1455						NA Since used as a Cond Heater
13	JH No 02 Condensate	Wilo	1	10	25	3	1455						
14	JH No 03 Condensate	KPD	1	55	25	10	1455	1	55	25	10	1455	Used for RJ3 rd Heating
15	JH No 04 Condensate	KPD	1	55	25	5	1455	1	55	25	5	1455	Used for CJ1/2 Heating
16	JH No 05 Condensate	Wilo	1	10	25	3	1455	1	10	25	3	1455	

17	JH No 06 Condensate	KPD	1	55	25			3	10	25	Suitable		Used for RJ3/SJ1/SJ2 Heater
18	Pan Cond Pump	KPD	3	55	25	Not given		3	55	25	Not given		IF HP suitable then existing used
19	Sulphured Juice	PSP	1	200	32	75	1475	2	300	60	75	1440	New 2 Pumps are required
		PSP	1	250	45	100	1480						
20	Clear Juice	KPD	2	175	30	75	1475	2	300	60	Suitable		New 2 Pumps are required
21	Filtrate Pump	KSB	2	150		10	1440	2	50	20	10	1440	Existing used IF Head Suit
22	Mud Pump	SHD	1	55	25	12.5	1440	2	55	25	12.5	1440	One Spare Pump of same capacity required
23	Pan Injection pump	KPD	1	1300	20	150	1478						Existing pumps used
		Sintech	1	1300	20	150	1478		5500	20			
		Sintech	2	2500	20	220	990						
24	Quadrauple Injection Pump	KPD	2	680	22	75	1480	2	680	22	75	1480	
25	Spray Pump	Sintech	2	2500	12	150	985	2	2500	12	150	985	2000M3/Hr 1 new pump required
			1	2000	12	150	985	2	2000	12	150	985	
26	Unsulphured Syrup	PSP	1	200	32	30	1460	1	200	32	30	1460	Existing pumps used
		PSP	1	200	32	25	1400	1	200	32	25	1400	
27	Sul Syrup Pump	Sintech	2	60	30	15	1450	2	60	30	15	1450	Existing pumps used
		SHD	1	55	25	15	1450	1	55	25	15	1450	

28	Lime Pump			Not Given				3	12	20	7.5	1440	New pumps required
29	Service Pump	KPD	3	NA				2	150	30	30	1480	If existng suitable use existing
30	A Masecuite pump	INDO	2	60	30	25	1440	2	60	30	25	1440	Existng pumps used
		PSP	1	50	30	25	1440	1	50	30	25	1440	
31	B Masecuite pump	PSP	2	20	30	15	1440	2	20	30	15	1440	Existng pumps used
		PSP	2	40	30			2	40	30			
32	C Masecuite		2	40	30	20	1440	2	40	30	20	1440	Existng pumps used
													For New pan suitable capacity pump is required with all accessories
33	B seed	PSP	1	30	30	15	1440	1	30	30	15	1440	Existng pumps used
			1	40	30	20	1440	1	40	30	20	1440	
34	CAW	PSP	1	30	30	15	1440	2	30	30	15	1440	one new pump of same capacity required
35	CFW	PSP	1	20	30	10	1440	2	20	30	10	1440	one new pump of same capacity required
36	C MVC Pump	PSP	1	20	30	15	1440	1	20	30	15	1440	Existng pumps used
37	B MVC Pump	PSP	1	20	30	15	1440	1	20	30	15	1440	Existng pumps used

38	A Heavy Pump	Hiflow	1	40	40	15	1440	1	40	40	15	1440	one new pump of same capacity required
39	A Light Pump	Hiflow	1	40	40	15	1440	1	40	40	15	1440	one new pump of same capacity required
40	B Heavy Pump	Hiflow	2	40	40	20	1440	2	40	40	20	1440	Exisitng pumps used
41	C Light Pump	Hiflow	1	40	40			1	40	40			Exisitng pumps used
42	Final Molasses	Hiflow	1	40	40			1	40	40			Exisitng pumps used
43	B Grain Feeding pump			Not Given									If Suitble capacity pump then exisitng used
44	Filter cake wash pump			Not Given				2	20	20	3	2850	

**R B PATIL**  
**TECHNICAL DIRECTOR**  
**R B PATIL & ASSOCIATES**